SAMPLE STUDY MATERIAL

Electronics Engineering EC/E&T



Postal Correspondence Course GATE, IES & PSUs Control System



A Team of IES & GATE Toppers

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	1. Transfer function, 4. Root locus 7. Compensator	2. Transient response 5. Nyquist plot 8. State space analysis	3. Stability 6. Bode plot 9. Miscellaneous	

CHAPTER-1

LAPLACE TRANSFORM

Let F be a function it's Laplace transform is denoted by $\Gamma(f)$. The Laplace transform f(s) of a

function f(t) is defined by

$$\Gamma(f) = f(s) = \int_0^\infty e^{-ts} f(t) dt$$

The integral is evaluated with respect to t, hence once the limits are substituted what is left are is term of s.

Derivation of Laplace Transform:

(1)
$$\Gamma(e^{at}) = \int_{0}^{\infty} e^{at} e^{-st} dt = \frac{1}{s-a}$$

1

(2)
$$\Gamma^{-1}\left(\frac{1}{s-a}\right) = e^{at}$$

(3)
$$f(t) = e^{at} \quad \text{put a = jon} \quad PLF \quad SAMPLE + 1$$

$$L\left(e^{jS}\right) = \frac{1}{s-jS} = \frac{1}{s-jS} = \frac{s+jS}{s^2+S^2}$$

$$L(\cos St + jSt) = \frac{1}{s-jS} = \frac{s+jS}{s^2+S^2}$$

$$L(\cos St + jSt) = \frac{s+jS}{s^2+S^2}$$

$$L(\cos St) = \frac{s}{s^2+S^2}$$

$$L(\cos St) = \frac{s}{s^2+S^2}$$

$$L(\sin St) = \frac{S}{s^2+S^2}$$

$$L(\sin St) = \frac{S}{s^2+S^2}$$

$$L^{-1}\left(\frac{s}{s^2+S^2}\right) = \cos St$$

$$L^{-1}\left(\frac{S}{s^2+S^2}\right) = \sin St$$

(4) In the function $f(t) = e^{at}$

$$a = -\Gamma + i\tilde{S}$$

$$a^{a} = e^{(-r+jS)t}$$

 $e^{at} = e^{(-r+jS)t}$ $f(t) = e^{(-r+jS)t}$

$$L\left(e^{(-\Gamma+j\tilde{S})t}\right) = \frac{1}{s - (-\Gamma+j\tilde{S})} = \frac{1}{(s+\Gamma) - j\tilde{S}}$$

$$e^{t-r+\beta S \mu} = e^{rr} (\cos S t + j \sin S t)$$

$$Le^{-rr} (\cos S t + j \sin S t) = \frac{1}{(s+r)-jS} = \frac{(s+r)+jS}{(s+r)^2+S^2}$$

$$L(e^{-rr} \cos S t) = \frac{s+r}{(s+r)+S^2} \qquad Le^{-rr} (\sin S t) = \frac{S}{(s+r)^2+S^2}$$

$$L^{-1} \left(\frac{s+r}{(s+r)^2+S^2}\right) = e^{-rr} \cos S t \qquad L^{-1} \left(\frac{S}{(s+r)^2+S^2}\right) = e^{-rr} \sin S t$$
(5) In the function f(t) = e^{it} put a = 1
f(t) = e^{t}
$$L(e^{t}) = \frac{1}{s-1}$$
Table of L.T
f(t) f(t) unit impulse at t = 0
(1) f(t) unit step at t = T
(2) u(t) unit step at t = T
(3) u(t) - trumit step at t = T
(4) t
(5) $\frac{1}{2}$

$$L^{-1} \frac{1}{s-1}$$
(6) t^n

$$\frac{1}{s} \frac{n}{s^{3}}$$
(7) e^{-rt}

$$\frac{1}{s} \frac{1}{s-a}$$
(8) e^{it}

$$\frac{1}{s-a}$$
(9) te^{-it}

$$\frac{1}{(s+a)^2}$$
(10) te^{it}

$$\frac{1}{s} \frac{1}{(s-a)^2}$$



(4) If the LT of
$$f(t)$$
 is $F(s)$ then $Le^{-at}f(t) = F(s + a)$

(5) if the LT of f(t) is F(s)

$$L(tf(t)) = -\frac{dF(s)}{ds}$$

(6) Initial value theorem

$$\lim_{t \to 0} f(t) = \lim_{s \to \infty} s L f(t) \qquad \lim_{t \to 0} f(t) = \lim_{s \to \infty} s F(s)$$
(7)
$$\lim_{t \to \infty} f(t) = \lim_{s \to 0} s L f(t) \qquad \lim_{t \to \infty} f(t) = \lim_{s \to 0} s F(s)$$

Q.1. Find the invercese LT of the following functions

(i)
$$F(s) = \frac{1}{s(s+1)}$$

 $L^{-1}\left(\frac{1}{s(s+1)}\right) = L^{-1}\left(\frac{1}{s}\right) - L^{-1}\left(\frac{1}{s+1}\right)$
 $L^{-1}\left(\frac{1}{s(s+1)}\right) = (1-e^{-t})$
(ii) $\frac{s+6}{s(s^2+4s+3)} + \frac{s+6}{s(s+1)} + \frac{s+6}{s(s+1)} + \frac{s+6}{s(s+1)} + \frac{s+6}{s(s+1)} + \frac{1}{s(s+1)} + \frac{1}{s+1} + \frac{1}{s+3} + \frac{1}{s+1} +$

Solution : We take the L.T of each term in given differential equation

$$s^{2}V(s) - sV(0) - V'(0) + 6[sV(s) - V(0)] + 8V(s) = \frac{2}{s}$$

$$V(0) = 1, \quad V'(0) = -2$$

$$s^{2}V(s) - s + 2 + 6[sV(s) - 1] + 8V(s) = \frac{2}{s}$$

$$V(s) = \frac{s^{2} + 4s + 2}{s(s+2)(s+4)} = \frac{A}{s} + \frac{B}{s+2} + \frac{C}{s+4}$$

$$A = sV(s)/_{s=0} = \frac{1}{4} \qquad B = (s+2)V(s)/_{s=-2} = \frac{1}{2} \qquad C = (s+4)V(s)/_{s=-4} = \frac{1}{4}$$

$$V(s) = \frac{\frac{1}{4}}{s} + \frac{\frac{1}{2}}{s+2} + \frac{\frac{1}{4}}{s+4}$$

by the Inverse L.T

$$V(t) = \frac{1}{4} (1 + 2e^{-2t} + e^{-4t})u(t)$$

Q.3. Solve for the response y(t) in the following integrodifferential equation

$$\frac{dy}{dt} + 5y(t) + 6\int_{0}^{t} y(\ddagger)d\ddagger = u(t)$$
$$y(0) = 2$$

Solution : Taking the LT of each term, we get



CHAPTER-2 BASICS OF CONTROL SYSTEM

Open–Loop Control System



In an open loop Control System the output is neither measured nor feedback for comparison with input. Faithfulness of an open loop control system depends on the accuracy of input calibration.

Closed-Loop Control System È



In a closed loop control system the output has an effect on control action through a feedback as shown figure and hence closed loop control systems are also termed as feedback control systems. The control action is actuated by an error signal e which is the difference b/w the input signal r and the output signal c. This process of comparison b/w the output and input maintains the output at a desired level through control action process.

Open Loop Systems

$$R(s) \longrightarrow C(s)$$

$$T.F. = \frac{C(s)}{R(s)} = G(s)$$

Closed Loop Systems



Figure-(a)

- 1. Automatic coffee server
- 2. Traffic Signal

ADVANTAGES È

3. Simple and economic

Disadvantages È

4. Unreliable

- 1. Electric Iron
- 2. D.C motor speed control
- 3. Accurate and reliable
- 4. The system is complex and costly

5. Inaccurate

Control System-EC

5. System may become unstable

From Figure-(a)	
C(s) = G(s).E(s)	(i)
E(s) = R(s) - B(s)	(ii)
B(s) = C(s)H(s)	(iii)
From (ii) and (iii) we have	

$$E(s) = R(s) - C(s).H(s)$$
(iv)

From (i) and (iv) we have

$$\frac{C(s)}{G(s)} = R(s) - C(s) \cdot H(s) \qquad \qquad R(s) = C(s) \left[\frac{1 + G(s)H(s)}{G(s)}\right] \qquad \qquad \frac{C(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)}$$

Modelling of a Control System

Translational Motion: Motion takes place along the horizontal or straight line to the section is called translational motion.



Where

B = damping coefficient

unit of B = N/m/sec.

3. Spring Force:

The restoring force of a spring is proportional to the displacement.

$$F_K(t) = Kx(t)$$

$$F = Kx$$

Unit of K = N/m

Where K = spring constant or stiffness

Stiffness = Restoring force per unit displacement.

ROTATIONAL SYSTEM:

The rotational motion of a body can be defined as the motion about a fixed point.

Force that resist motion:

1. Inertia Torque:

$$T_1 = J \cdot \frac{d^2_{"}(t)}{dt^2}$$

 $_{"}(t) =$ Angular velocity

J = moment of inertia

2. Damping Torque:

The damping torque $T_D(t)$ is the product of damping coefficient B and angular velocity ω .

$$T_{D}(t) = B\tilde{S}(t)$$

$$T_{D}(t) = B.\frac{d}{dt}, (t)$$

$$T = B.\frac{d}{dt}$$

$T = K_{"}$

Unit of K = N.m/rad.

D'Alebert's Principle:

The principle states that " for any body the algebraic sum of all forces is equal to zero" i.e. Applied force + Resisting force = 0

Example 1:

Inertia force
$$= F_1 = M \frac{d^2 x}{dt^2}$$

Damping force $= F_2 = f \cdot \frac{dx}{dt}$





L

V

Spring force $= F_3 = Kx$

From D'Alembert's principal

$$F = F_1 + F_2 + F_3$$

$$F = M \frac{d^2 x}{dt^2} + f \frac{dx}{dt} + kx \qquad \dots (1)$$

i.e. Applied force = Resisting force.

Procedure of Writing the Equations for Mechanical Systems:

- 1. Consider the system is in equilibrium
- 2. Same arbitrary displacement
- 3. Draw a free body diagram for each mass.
- 4. Apply Newton's law of motion on each diagram
- 5. Write the equation in suitable form

Force Voltage Analogy:

Consider the circuit shown below.



$$V_{in} = L\frac{d^2q}{dt} + \frac{R.dq}{dt} + \frac{q}{c} \qquad \dots \dots (2)$$

From example-1 on comparing equation (1) and (2) are can write.

Electrical	Analogous to	Mechanical
L	Analogous to	М
R	Analogous to	f
К	Analogous to	1/C
V_{in}	Analogous to	Force
Q	Analogous to	Displacement 'x'

FORCE CURRENT ANALOGY:

Consider the circuit shown below.



Apply K.C.L.

$$i = \frac{V}{R} + \frac{1}{L} \int v dt + C \cdot \frac{dV}{dt}$$

Since $v = \frac{dW}{dt}$
 $i = \frac{Cd^2W}{dt^2} + \frac{1}{R} \cdot \frac{dW}{dt} + \frac{W}{L}$

On comparing with the equation (1) of example 1(a) we can write.

Electrical	Analogous to	Mechanical
С	"	М
1/R	"	f
1/L	"	K
φ	"	Х
I	"	force

Note: We can represent any mechanical system to a electrical system or vice-versa by the use of modelling.



 $N_1 \& N_2$ = No. of teeth on wheels

Consider ideal case

Work done by wheel 'a' = work done by wheel 'b'

$$\therefore \qquad T_1 Q_1 = T_2 Q_2$$

$$\boxed{\frac{T_1}{T_2} = \frac{Q_2}{Q_1}} \qquad \dots \dots (i)$$

And linear distance will be

$$\frac{Q_1}{Q_2} = \frac{r_2}{r_1}$$

 V_2

$$\therefore \qquad \overline{\frac{T_1}{T_2} = \frac{Q_2}{Q_1} = \frac{r_1}{r_2}}$$

.....(ii)

Since the n.o. of teeth is proportional to radius. Thus

$$\frac{N_{1}}{N_{2}} = \frac{r_{1}}{r_{2}}$$
And $\frac{w_{1}}{w_{2}} = \frac{Q_{2}}{Q_{1}}$
So
$$\frac{\overline{T}_{1}}{T_{2}} = \frac{Q_{2}}{Q_{1}} = \frac{r_{1}}{r_{2}} = \frac{N_{1}}{N_{2}} = \frac{w_{2}}{w_{1}}$$
....(iii)
From force-voltage analogy
Where
$$V_{1} \rightarrow \text{ is analogous to } \rightarrow T_{1}$$

$$V_{2} \rightarrow \text{ is analogous to } \rightarrow T_{2}$$

$$I_{1} \rightarrow \text{ is analogous to } \rightarrow N_{1}$$

$$r_{2} \rightarrow \text{ is analogous to } \rightarrow N_{2}$$
From force-vurrent analogy
$$I_{1} \qquad I_{2} \qquad V_{1} \qquad I_{2} \qquad V_{1} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{2} \qquad V_{2} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{1} \qquad V_{2} \qquad V_{2}$$

Question: Show the electrical connection diagram and model the armature controlled d.c. motor in a block diagram form. Assume the necessary variables and obtained transfer function for change in

position of armature to the change in armature voltage. Express the transfer function in standard form.

 $N_1' = N_2'$

IES-2011-EE

Solutions: Armature Controlled d.c. Motor



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Figure

Consider the armature controlled d.c. motor and assume that the demagnetizing effect of armature reaction is neglected, magnetic circuit is assumed linear and field voltage is constant i.e. $I_f = constant$

Let R_a = Armature resistance

 L_a = Armature self inductance caused by armature flux

 i_f = field current

E = **Induced e.m.f in armature**

V = **Applied voltage**

T = Torque developed by the motor

 θ = Angular displacement of the motor shaft

J =Equivalent moment of inertia of motor shaft & load referred to the motor

B = equivalent coefficient of friction of motor and load referred to the motor Apply KVL in armature circuit



Now, the torque T delivered by the motor will be the product of armature current and flux

Trwi_a

$$T = K i_a \qquad \dots \dots (3)$$

Where K = motor torque constant

The dynamic equation with moment of inertia & coefficient of friction will be

$$T = J \frac{d^2_{"}}{dt^2} + B \frac{d_{"}}{dt} \qquad \dots \dots (4)$$

Take the Laplace transform of equations 1, 2, 3 and 4

$$V(s) - E(s) = I_a(s)(R_a + SL_a)$$
$$E(s) = K_b S_u(s)$$

$$T(s) = K I_a(s)$$

$$T(s) = (s^2 J + sB)_{\prime\prime}(s)$$

$$T(s) = (SJ + B)S_{"}(s)$$

The block diagram for each equation



Combine all four block diagrams



Equation 5 can be written as

$$\frac{I_{a}(s)}{V(s)} = \frac{K}{R_{a}\left(1 + s\frac{L_{a}}{R_{a}}\right)sB\left(1 + s.\frac{J}{B}\right) + KK_{b}s}$$

Put $\frac{L_a}{R_a} = \ddagger_a$ time constant of armature circuit

 $\frac{J}{B} = \ddagger_m =$ Mechanical time constant

Equation 5 becomes

$$\frac{W(s)}{V(s)} = \frac{K}{sR_aB(1+s^{\ddagger}_a)(1+s^{\ddagger}_m) + KK_bs} \qquad \dots \dots (6)$$

From the block diag. figure it is clear that it is a closed loop system. The effect of the back e.m.f is represented by the feedback signal proportional to the speed of the motor.

77	Final	Selections in Engineeri	ng Services 2014.	
Rank	Roll	Name	Branch	
1	171298	SAHIL GARG	EE	
3	131400	FIRDAUS KHAN	ECE	
6	088542	SUNEET KUMAR TOMAR	ECE	
8	024248	DEEPANSHU SINGH	EE	
10	207735	VASU HANDA	ECE	
22	005386	RAN SINGH GODAN	ECE	
22	032483	PAWAN KUMAR	EE	
29	070313	ARABA ROYAL	EXA	
31	214577	PRAMOD RAWANI	EE	
33	075	DIPTERANJAN (TRIJATIV	E	
35	003853	SHANKAR GANESH K	ECE	
35	1781	KOUSHIK PAN	Le LE	
36	052187	ANOOP A	ECE	
37	008283	ARPIT SHUKLA	ECE	
38	106114	MANISH GUPTA	EE	
41	018349	AIRAN CHEROLOGICAL	ECE	
44	098058	LEENA P MARKOSE	EE	
45	029174	NAVNEET KUMAR KANWAT	EE	
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